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Choosing specifications for plastering

With the help of tabulated summaries, this digest shows how the main factors affecting the choice of suitable plastering specifications can be made in logical sequence.
It replaces Digest 49 which is now withdrawn.

Plastering is intended to conceal unevenness in the background, and to provide a finish that is smooth, crack-free, hygienic, resistant to damage and easily decorated. It may also be required to improve fire resistance, to provide additional thermal and sound insulation, to modify sound absorption or mitigate the effects of condensation; but where these are of secondary importance, as is usually the case, the selection of a plastering specification will depend first upon the surface finish desired. The stages in choosing plastering specifications will therefore be considered from this starting point.

Stage 1

Choosing the finish

The quality of the plaster finish, whether it should be hard or soft, smooth or textured, and also the choice of the decorative coating and the time likely to be available for drying out the plaster before the finish can be applied, will usually be the main considerations. The finish may also have to meet special requirements concerning sound absorption or condensation. Table 1 lists plastering systems suitable for various backgrounds and Table 2 lists plaster finishes and sets out the more important properties likely to determine their choice. For ease of reference in Table 1, most of the finishes have been designated as Categories I to VI in Table 2.

Stage 2

Number of coats

At one time, three-coat plasterwork was applied to most backgrounds: a first, levelling undercoat, followed by a second undercoat to provide uniform suction for the finishing coat. Nowadays, the surface of brickwork and blockwork is such that two-coat work is usually possible, though it is more important than ever, given a regular surface, to avoid extreme variations of suction. Some backgrounds, such as plasterboard and smooth concrete, have level surfaces and uniform suction which make single-coat plastering possible. In this context, the references in Table 1 to 'sufficiently level' backgrounds require explanation. Different plasters are able to tolerate surface irregularities to different extents; this is because of the different thicknesses of one-coat plasters normally applied. Thin-wall plasters based on organic binders are usually no more than 1.5 mm thick to be economic. Holes and scratches in the background must therefore be filled in by hand before a finish of this thickness can be applied. Thin-wall plasters based on gypsum are thicker (up to 5 mm) and so are more tolerant of blemishes. Single-coat board finish gypsum plasters may range from 3 mm thickness on solid backgrounds (see Table 1) to 5 mm on plasterboard or plaster lath.

It is not necessarily true that two-coat work is superior to single-coat work. The use of single-coat plastering on plasterboard does tend to increase the

Prepared at Building Research Station, Garston, Watford, WD2 7JR
Technical enquiries arising from this Digest should be directed to Building Research Advisory Service at the above address.

Table 1 Suitable plastering systems for various backgrounds

The numbers in parentheses correspond to the numbered notes in the text

Background					Suitable alternative undercoat plasters						
Class (1)	Type	Suction (2)	Key or bond (3)	Drying (4)	Type of finish (5)	Premixed lightweight plasters		Sanded browning plasters (proportions by volume) (2a and 2b)	Undercoats based on cement (proportions by volume)	Remarks	Single-coat work (excluding projection plaster) (6)
						Gypsum (2c)	Cement				
Solid	Normal clay brickwork and blockwork	Moderate to high	Good if joints well raked or bricks keyed	Negligible	I Gypsum/lime II Weak lime III Lightweight IV Cement V Projection	— — Browning — —	— Backing Backing — —	1 : 3 1 : 3 — — —	1 : 1 : 6 1 : 1 : 6 or 1 : 2 : 9 — 1 : ¼ : 3, 1 : 1 : 6 or 1 : 2 : 9 —	Background should be dry to minimise efflorescence	Not suitable for this type of background
	Dense clay brickwork (other than engineering brickwork) and calcium silicate or concrete blockwork or brickwork	Low to moderate	Variable; bonding treatments may be required for cement based undercoats	Low to high for materials other than clay brickwork	I Gypsum/lime II Weak lime III Lightweight IV Cement V Projection	— — Browning or bonding — —	— Backing Backing — —	1 : 2 1 : 2 — — —	1 : 1 : 6 1 : 1 : 6 or 1 : 2 : 9 — 1 : ¼ : 3, 1 : 1 : 6 or 1 : 2 : 9 —	Background should be dry to minimise shrinkage except for dense clay brickwork	Not suitable for this type of background
	Clay engineering brickwork, dense concrete	Low	Hacking, spatterdash or bonding treatment may be needed	Negligible for clay brickwork, low to high for dense concrete	I Gypsum/lime II Weak lime III Lightweight IV Cement V Projection	— — Bonding — —		1 : 1½ 1 : 1½ — — —	1 : 1 : 6 1 : 1 : 6 or 1 : 2 : 9 — 1 : ¼ : 3, 1 : 1 : 6 or 1 : 2 : 9 —		Sufficiently level concrete surfaces may be plastered with thin-wall plasters or board finish plasters: a bonding treatment may be necessary
	No-fines concrete	Low	Good	Low to moderate	I Gypsum/lime II Weak lime III Lightweight IV Cement V Projection	— — Browning — —	— Backing Backing — —	1 : 2 1 : 2 — — —	1 : 1 : 6 1 : 1 : 6 or 1 : 2 : 9 — 1 : ¼ : 3, 1 : 1 : 6 or 1 : 2 : 9 —		Not suitable for this type of background
	Close textured lightweight aggregate concrete blocks	Low	Poor; bonding treatments may be necessary	Moderate to high	I Gypsum/lime II Weak lime III Lightweight IV Cement V Projection	— — Bonding — —	— Backing Backing — —	1 : 1½ 1 : 1½ — — —	Not normally suitable for this type of background	Background should be dry to minimise shrinkage movement	Sufficiently level surfaces may be plastered with thin-wall plasters or board finish plasters: a bonding treatment may be necessary
	Open textured lightweight aggregate concrete blocks	Low to moderate	Good	Moderate to high	I Gypsum/lime II Weak lime III Lightweight IV Cement V Projection	— — Browning — —	— Backing Backing — —	1 : 2 1 : 2 — — —	1 : 1 : 6 1 : 1 : 6 or 1 : 2 : 9 — Not suitable —	Background should be dry to minimise shrinkage movement	Not suitable for this type of background

Background					Suitable alternative undercoat plasters						
Class (1)	Type	Suction (2)	Key or bond (3)	Drying shrinkage (4)	Type of finish (5)	Premixed lightweight plasters		Sanded browning plasters (proportions by volume) (2a and 2b)	Undercoats based on cement (proportions by volume)	Remarks	Single-coat work (excluding projection plaster) (6)
						Gypsum (2c)	Cement				
Solid	Aerated concrete slabs and blockwork	Moderate to very high	Poor: bonding treatments may be necessary	Moderate to high	I Gypsum/lime	—	—	1 : 2	1 : 1 : 6	Some blocks of very high suction may require special plasters of high water retentivity or sealing with a bonding agent	Sufficiently level surfaces may be plastered with thin-wall plasters or board finish plasters: a bonding treatment may be necessary
					II Weak lime	—	Backing	1 : 2	1 : 1 : 6 or 1 : 2 : 9		
					III Lightweight	Browning or HSB Browning	Backing	—	—		
					IV Cement	—	—	—	1 : 1 : 6 or 1 : 2 : 9		
					V Projection	—	—	—	—		
	Any surface treated with a bonding agent: for example glazed bricks, tiled or sound painted surfaces all treated with bonding agents	Low	Poor: bonding treatments necessary	Usually negligible	I Gypsum/lime	—		1 : 1½	Not suitable for this background		Sufficiently level surfaces may be plastered with thin-wall plasters: a bonding treatment may be necessary
					II Weak lime	—		1 : 1½			
					III Lightweight	Bonding		—			
					IV Cement	—		—			
					V Projection	—		—			
Slab	Wood wool slabs	Low	Good	Usually fixed dry, but may be high when used as permanent shuttering	I Gypsum/lime	—	—	1 : 2	—		Not suitable for this type of background
					II Weak lime	—	Backing	1 : 2	1 : 2 : 9		
					III Lightweight	Metal lathing	Backing	—	—		
					IV Cement	—	—	—	1 : 2 : 9		
					V Projection	—	—	—			
Board	Plasterboard	Low	Adequate with suitable plasters	Fixed dry	I Gypsum/lime	—		1 : 1½	Not suitable for this background		Sufficiently level surfaces may be plastered with board finish plasters
					II Weak lime	—		1 : 1½			
					III Lightweight	Bonding		—			
					IV Cement	—		—			
					V Projection	—		—			
	Expanded plastics boards	Low	Adequate with suitable plasters	Fixed dry	I Gypsum/lime	—		1 : 1½	Not suitable for this background	Not suitable for paper faced laminates	If the boards are fully bonded to a firm background sufficiently level surfaces may be plastered with board finish plasters
					II Weak lime	—		1 : 1½			
					III Lightweight	Bonding or metal lathing		—			
					IV Cement	—		—			
					V Projection	—		—			
Lathing	Metal lathing	Low	Good	None	I Gypsum/lime	—	—	1 : 1½ followed by 1 : 2	1 : 1 : 6	Three coats required. Metal lathing should be well braced. Mixes for first undercoat should contain hair or fibre. Lathing to receive spray application available	Not suitable for this type of background
					II Weak lime	—	Backing	—	1 : 1 : 6 or 1 : 2 : 9		
					III Lightweight	Metal lathing	Backing	—	—		
					IV Cement	—	—	—	1 : 1 : 6 or 1 : 2 : 9		
					V Projection	—	—	—	—		

Table 2 Characteristics of plaster finishes

Category in Table 1	Plaster finish	Surface hardness and resistance to impact damage	Other surface characteristics	Restrictions on early decoration	Shrinkage or expansion	Remarks
II	*Lime plasters* Lime	Weak and very easily indented	Open-textured (depending on sand), absorbs condensation	Initially only suitable for permeable finishes that are unaffected by alkali	Shrink on drying, but shrinkage is reduced by addition of fine sand	Slow hardening. Only apply on dry undercoats
II	Gauged lime	Resistance to damage increases with proportion of gypsum plaster	Similar to above, but smoother finishes obtainable		Shrinkage is restrained by the gypsum content provided that over-trowelling is avoided	Only apply on dry undercoats
I	*Gypsum plasters* Class D (Keenes)	Very hard and resistant to damage	Very level and smooth. Particularly suitable for low-angle lighting conditions	None, except on undercoats containing cement or lime, or unless lime is added to the finishing coat	Expand during setting. Subsequent movements usually small, but too rapid drying can lead to delayed expansion	Set slowly and so allow ample time for finishing to a smooth surface. Should not be allowed to dry too quickly
I	Class C (anhydrous)	Hard and resistant to damage	Slightly less smooth than Class D			
I	Class B (hemihydrate)	Sufficiently hard and resistant for most normal purposes, but weakened by additions of lime	Sufficiently smooth and level for most purposes		Expand during setting, though extremely slightly with board finish plasters. Subsequent movements are small	Set quickly, should be allowed to dry as soon as possible
III	Lightweight	Surface hardness similar to Class B plasters. Ease of indentation varies with the type of lightweight undercoat, but resilience tends to prevent serious damage	Sufficiently smooth and level for most purposes	None, but the higher water content of lightweight undercoats makes these somewhat slower to dry than sanded gypsum plaster undercoats	Expand during setting. Subsequent movements usually small and easily restrained by background	Maximum fire resistance. Lightweight plaster surfaces warm up more quickly than others and so help to prevent temporary condensation
IV	*Cement/lime/sand* 1 :0–¼ :3	Very strong and hard	Wood float finish	Initially only suitable for permeable finishes that are unaffected by alkali	Shrink on drying, but surface cracking can be minimized by avoiding over-working	Suitable for damp conditions
IV	1 :1 :6	Strong and hard	Wood float finish			
IV	1 :2 :9	Moderate	Wood float finish			
I	*Single-coat finishes* Board finish gypsum plasters (Class B)	Surface hardness similar to Class B above, but resistance depends on background	On suitable backgrounds, similar to Class B above	None ; finish dries very quickly	Extremely small expansion on setting. Subsequent movements small	
VI	*Thin-wall finishes* Based on gypsum	Softer than board finishes	Smooth and level on sufficiently level backgrounds	Dries very quickly. No restrictions when dry	Extremely small expansion on setting. Subsequent movements small	
VI	Based on organic binders	Moderately hard. Resistance depends on background	Matt surface, closely following the level of the background	Dries very quickly. No restrictions when dry	The very thin coats are restrained by the background	
V	Gypsum projection plasters	Properties generally intermediate between Class B and Class C gypsum plasters				

risk of cracking at the joints, as compared with two-coat plastering, but it is better on surfaces of smooth concrete or painted surfaces treated with a bonding agent: the thinner plaster is less likely to fail in adhesion as a result of differential thermal movement. Another advantage of single-coat plastering on dry backgrounds, such as precast concrete slabs or boards, is that it considerably reduces the quantity of water introduced during the later stages of construction. The thin plaster dries very quickly and there is no restriction on the type of decoration.

Although gypsum projection plasters are applied as a single coat, the thickness may range from 5 mm to 25 mm depending on the mechanical key and suction of the background. The previous comments on the properties of single-coat work will therefore apply only to the thinner coats of this plaster.

Stage 3

Plaster undercoats

As long as proper attention is given to the selection of plaster undercoats to match the suction of the background, its surface irregularities and other important properties, a wide range of finishes is possible, whatever the background. Rarely does the plaster finish required determine the background. Table 1 sets out the properties of backgrounds that determine which undercoats should be used or whether single-coat work is possible, and indicates suitable alternative plastering systems for each background. Notes on the use of Table 1 are given below, describing these properties in more detail; the reference numbers that precede these notes correspond to the reference numbers in the table.

(1) Strength of background

This is particularly important where undercoats based on cement are to be used; the strength of the background must be adequate to restrain their drying shrinkage. Undercoats based on gypsum plasters do not shrink appreciably on drying, so that unless the background itself is likely to shrink after these undercoats are applied considerations of strength are unimportant.

(2) Suction of background—strength, adhesion and quality of plaster work

Strength

(2a) The appropriate ratio by volume of plaster to Type 1 sand (BS 1198–1200) in sanded browning plasters will be seen from Table 1 to vary from 1 :3 (for backgrounds of moderate to high suction) to 1 :1½ for low-suction backgrounds. The higher the sand content of the plaster, the greater the amount of water needed to make the mix workable. The 1 :3 mix would give too weak a plaster unless the background removes some of the water before the plaster sets. A high-suction background reduces the water/plaster ratio (and hence increases the strength of the set material) to much the same level as that of a 1 :1½ mix applied to a low-suction background.

(2b) When Type 2 sands are used instead of Type 1, the proportions of sand in all sanded browning plasters should be reduced by one-third below the figures given in Table 1. This is because finer sands require more water to obtain a workable mix. Too much water leads to a loss of strength in the plaster, hence the need to reduce the sand content if finer sands are used.

(2c) The proportions of gypsum plaster in ready-mixed lightweight gypsum undercoat plasters have been similarly designed to match the suction of particular backgrounds. The proportion of plaster in the welterweight bonding plaster is higher than in the ordinary lightweight gypsum bonding coat plaster, so that it is heavier, stronger and more easily worked. It is, however, suitable for the same backgrounds.

Adhesion A background of very high suction, eg aerated concrete or insulating bricks, may absorb water so rapidly from the plaster mix that its adhesion to the background is weakened; there may also be too little time in which to level the coat. To deal with this problem by excessive wetting of the background before plastering is to invite risk of trouble later on from drying shrinkage, efflorescence or spoiled decorations. It is better to use mixes which retain their water in contact with backgrounds of high-suction. Plasters containing lime can be improved by using a fat lime putty rather than dry hydrated lime or by mixing in a high-speed mixer. Alternatively, proprietary plasters (eg high-suction browning) are available which derive their improved water-retaining properties from cellulose additives, and such additives may also be used to improve the adhesion and 'workability' of aerated cement-sand mixes.

Quality It is often difficult to obtain a satisfactory plaster finish on backgrounds comprised of more than one material because of their uneven suction. Differential suction is a common occurrence with block walls and 'grinning' through of the joints is not uncommon, particularly with single-coat work or when an unduly thin undercoat is used in two-coat work. Most commonly, the difficulties occur with aerated concrete blocks, due to their suction being high in comparison with that of the mortar joints. This difference can be reversed when walls built of lightweight aggregate concrete blocks that have become very wet in the stack are plastered soon after construction. The blocks then have virtually no suction, whilst the mortar joints have moderate suction. An undercoat of a lightweight gypsum browning plaster applied to such a wall tends to remain soft over the blocks but to stiffen over the joints and to build up to a slightly greater thickness there as it is worked. The resulting difference in level is not corrected by the final coat, and can be of the order of 1 to 2 mm. This effect can be prevented by not plastering on unduly wet walls and by ensuring that undercoats are of the full recommended thickness. It emphasises the good practice of storing blocks under cover.

(3) Key or bond

While high-suction backgrounds can have an immediate effect upon the adhesion of plaster, as discussed above, the continuing adhesion of the plaster is dependent upon the key or bond provided. The adhesion is threatened by the stresses which can develop between the plaster and the background as a result of differences in thermal expansion or drying shrinkage. The key or bond must therefore be adequate to contain these stresses, which can be such as to cause failure in plaster otherwise able to withstand a tensile stress of 0.7 MN/m^2. The preparation, the key or bonding agent, and the plaster, can all be chosen to minimise risk of failure from this cause. The greater elasticity of lightweight plasters helps to reduce stresses. The thickness of plaster coats should not appreciably exceed the recommendations of BS 5492 because shear stress is directly proportional to thickness, and the good mechanical key of metal lathing or wood-wool should be fully utilised by working the plaster well into the interstices with the trowel.

With backgrounds offering little or no key, such as smooth concrete, the choice of undercoat is more restricted but bonding agents applied to the background surface before plastering can considerably improve adhesion in these instances.

The PVAC emulsion type of bonding agent is particularly of value for dense concrete containing brick, granite or limestone aggregate, and for some structural lightweight concrete. This type of bonding agent is also useful in controlling the suction of backgrounds or dry undercoats. The bituminous type can be advantageous on walls where it is required to resist damp penetration but it is not recommended for use on soffits.

(4) Drying shrinkage and thermal movement

These movements have been mentioned above but some points of detail are better dealt with separately. As noted in Table 1, the shrinkage of clay brickwork or blockwork is low compared with that of concrete blockwork and other products based on cement. With the latter, therefore, it is particularly necessary to allow them to dry out as completely as possible before plastering.

The high drying shrinkage of wood-wool slabs causes little trouble when the slabs are fixed dry and are restricted by their fixing. But if they are used as permanent shuttering for casting concrete the slabs get wet and subsequent drying shrinkage can cause serious cracking of the plaster unless it is strong enough to restrain the movement.

Thermal movements of backgrounds are rarely large enough to cause serious defects, except in concrete roofs and heated concrete floors. Precautions are discussed later to prevent cracking of plaster at the junctions of walls and ceilings.

Some backgrounds of smooth-surfaced concrete (see Note 3) have negligible coefficents of expansion compared with that of gypsum plaster. Differential thermal movement is then not only much greater than normal, but the smooth surface of the concrete offers little key to the plaster to restrain the movement. Bonding agents of the PVAC emulsion type will strengthen the bond in these instances and also control the suction of the background if this is excessive. Alternatively, plasters with improved water-retaining properties can be used.

Efflorescence

Ideally, backgrounds should be dry before plastering but if not, the plaster should be allowed to dry before decorating. Any efflorescence can then be brushed off before the decorations can be spoiled. As long as the background remains dry there should be no further efflorescence.

Backgrounds are, however, frequently plastered before they have dried out, and if they are likely to contain efflorescent salts (as may clay brickwork and clay blockwork, for example) it is advisable to choose an undercoat that will present a barrier to them. For this purpose, undercoats based on cement are preferred to those based on gypsum plaster. Aerated cement/sand undercoats are more effective than cement/lime/sand undercoats.

Stage 4

Plastering specification

Tables 1 and 2, with the assistance of the preceding notes, should enable an appropriate type of finish to be selected for a given background. Some further notes are given here on the constitutions of these plasters and on the application of the other finishes described in Table 2.

(5) Type of finish

I Gypsum Any class B or class C gypsum plaster, neat or gauged with not more than ¼ volume of lime. Keene's plaster final coats are not included in this category since they are stronger than other gypsum finishes and require stronger undercoats. Traditionally, a 1 :3 Portland cement/sand undercoat is used, but this is suitable only for strong backgrounds with good mechanical key, eg brickwork or no-fines concrete. A 1 :1 class B hemihydrate gypsum plaster/sand undercoat may be used on some other backgrounds, but the manufacturer should be consulted as to its suitability for this purpose.

I Moderately strong lime A final coat of lime putty gauged with more than half its volume of gypsum plaster. Fine sand may be added to this up to an amount equal to the volume of lime putty.

II Weak lime This category is restricted to the weaker finishes of lime putty gauged with up to half of its volume of gypsum plaster, to which up to 1 volume of fine sand may be added. The stronger lime finishes, of lime putty gauged with ½ to 1 volume of gypsum plaster, should be used only with the stronger undercoats recommended for neat gypsum final coats.

III Lightweight Any of the proprietary finishes usually recommended for use on lightweight gypsum plaster undercoats.

IV Cement Final coats as for cement-based undercoats. The cement/lime/sand mixes are normally somewhat easier to float to an acceptable finish than are the corresponding aerated mixes.

In all cases mixes should not be stronger than the backing to which they are applied.

Alternative mixes for cement/lime/sand undercoats and final coats are described in Table 3.

V Gypsum projection plasters A blend of gypsum plasters which has been specially formulated for use with mechanical plastering machines that mix and spray the plasters as a direct one coat application. The plasters are then levelled and trowelled by conventional methods. Two grades of plaster are available. A multi-purpose grade is for general use to most internal high and low suction backgrounds and an ordinary grade is only intended for use on low suction backgrounds. The plasters are not suitable for certain types of background and the advice of the plaster manufacturer should be sought.

VI Thin-wall plasters These include the so-called Scandinavian plasters commonly applied either by spraying or with a broad spatula, and the finishing plasters of high water retention designed for high-suction backgrounds.

Alternative specifications for gypsum plaster or lime finishes (Categories I and II)

Table 1 shows that for several backgrounds there is a choice between two undercoats based on cement, and a third of sanded gypsum browning plaster, as alternative specifications with gypsum plaster or lime finishes. (In addition, undercoats of lime/sand gauged with gypsum plaster, in a volume ratio class 'B' browning plaster to lime to sand of 1 :3 :9, can receive weak lime finishes and may, subject to the following precautions, be substituted for a 1 :2 :9 cement/lime/sand undercoat wherever this is indicated in the table).

If the background is salt-free and likely to remain dry, gypsum has the advantage over cement-based undercoats in drying out and hardening quickly, and enabling application of the finishing coat to be made in less than 24 hours. However, the advantage of speed in plastering is lost if efflorescence delays or spoils decorations, and in these circumstances, as explained under *Efflorescence*, it is better to use cement-based undercoats. The choice then lies between cement undercoats plasticised by lime or by air-entraining mortar plasticisers. An aerated mix does not develop the high suction of lime-plasticised mixes and is a more effective barrier to efflorescent salts; but if aerated mixes are applied in cold and humid conditions, they may be slow to develop even the little suction needed to ensure satisfactory adhesion of the finish. Further, aerated mixes are less easily pumped for spray-plastering purposes than cement/lime/sand mixes.

Design of plasterwork to prevent cracking

The causes and prevention of cracking in plaster have been largely covered in the preceding notes. To prevent cracking over the joints between board and slab backgrounds other precautions are necessary, however. The plaster there can be reinforced with jute scrim or metal mesh and should be of adequate strength and thickness.

Discontinuities in backgrounds, eg where brickwork abuts concrete, are likely to cause cracking because of differential thermal expansion and drying shrinkage. At these positions the plaster should, if possible, be cut through, and the cut may then be masked by a cover strip fixed to one side. Alternatively, the plaster can be isolated from the background for some distance on both sides of the discontinuity and held instead on metal mesh or lathing. For pier and panel construction this isolation may be provided by means of building paper or polyethylene sheeting, and the reinforcing metal lath is fixed to the panels on both sides. This method has the effect of providing an appreciable width of isolated plaster which can accommodate the differential movement elastically, without cracking.

Junctions between walls and ceilings can be covered by cornices that will tolerate slight movements without cracking. Alternatively, a straight cut can be made through the wall plaster to isolate it from the effects of shrinkage at the joints.

Table 3 Cement-based plaster mixes (proportions by volume)

Cement/lime/sand	Cement/ready-mixed lime/sand		Cement/sand (using air entraining agent)	Masonry cement/sand
	Ready-mixed lime/sand	Cement/ready-mixed material		
1 :¼ :3	1 :12	1 :3	—	—
1 :½ :4 to 4½	1 :8 to 9	1 :4 to 4½	1 :3 to 4	1 :2¾ to 3½
1 :1 :5 to 6	1 :6	1 :5 to 6	1 :5 to 6	1 :4 to 5
1 :2 :8 to 9	1 :4½	1 :8 to 9	1 :7 to 8	1 :5½ to 6½

Standards and Codes

The various factors that should be considered when selecting a plastering specification are dealt with in greater detail than in this digest in British Standard Code of Practice BS 5492:1977, Internal plastering.

Further information may also be obtained from the following British Standards:

BS 12	Portland cement
BS 146	Portland-blastfurnace cement
BS 405	Expanded metal (steel)
BS 890	Building limes
BS 1142	Fibre building boards
BS 1191	Gypsum building plasters
BS 1198–1200	Building sands from natural sources
BS 1230	Gypsum plasterboard
BS 1369	Metal lathing (steel) for plastering
BS 2552	Polystyrene tiles for walls and ceilings
BS 4471	Dimensions for softwood, Part 2: Small re-sawn sections

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